



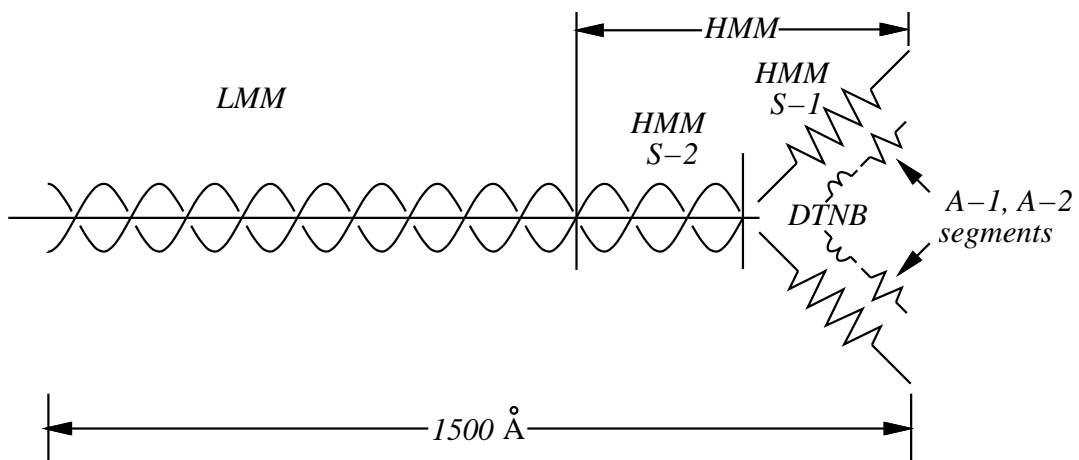
Actuators

...physical devices that transform electrical, chemical, or thermal energy into mechanical energy...

- electric
 - stepper motors
 - permanent magnet DC motors
- hydraulic
- pneumatic
- artificial muscles
 - shape memory alloys
 - polymers
 - protein-based actuators
 - bucky tubes
- muscle



Muscle: Contractile Proteins

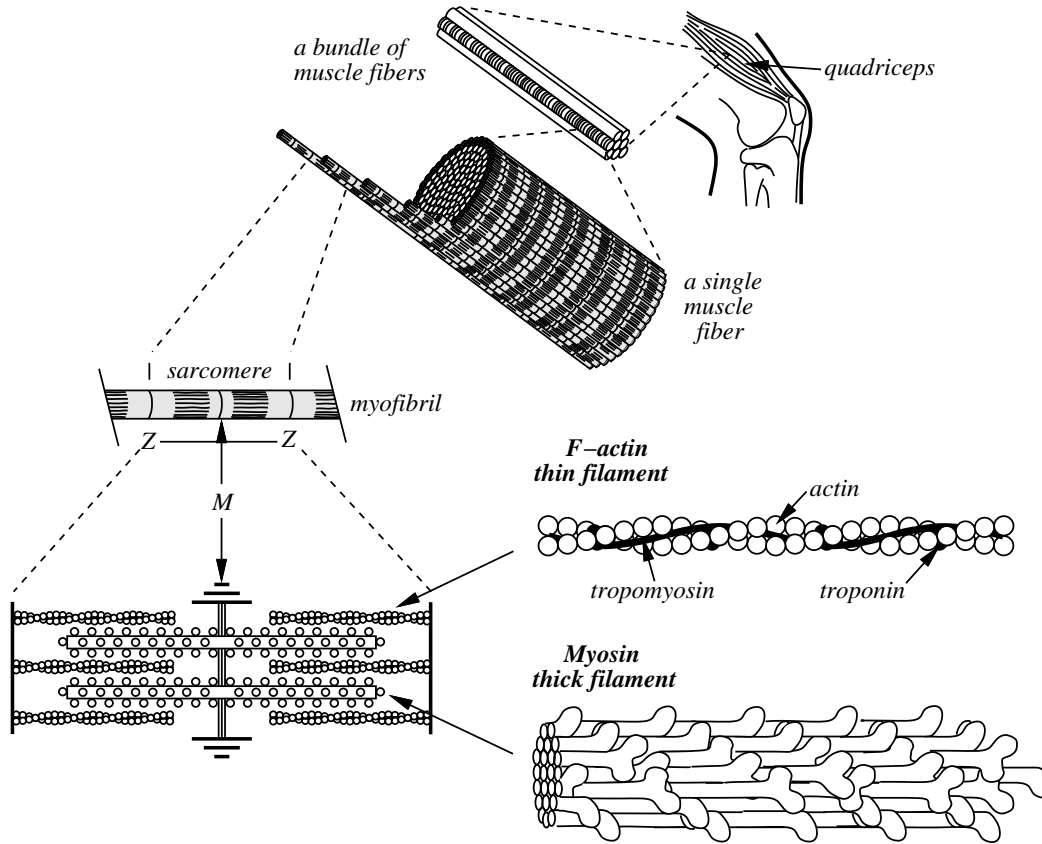


[adapted from Wilkie 1974, McMahon 1984]

Myosin molecules consist of multiple molecular subchains that participate in specialized roles.



Muscle: Sliding Filament Model

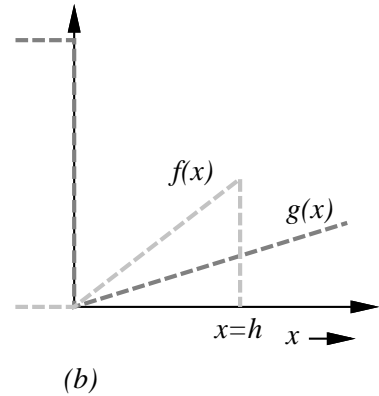
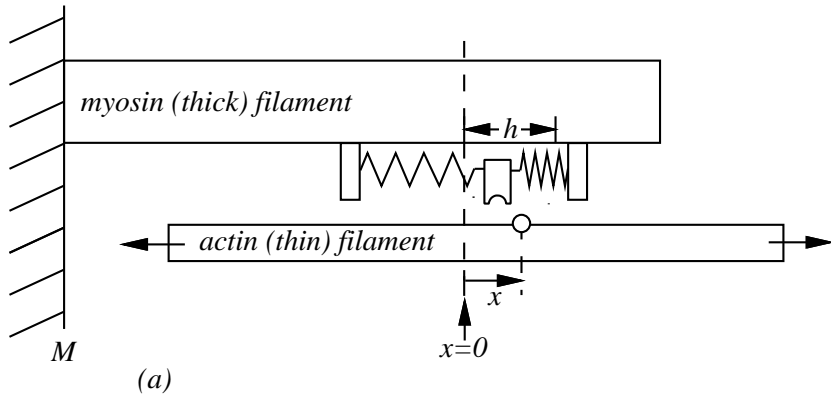


[adapted from McMahon 1984]

- Neural stimuli causes actin to bind free Ca^{++} ions and thus prepare attachment sites for the S-1 subchain of myosin
- because of attachment, the head of the myosin changes shape and angle of attachment, producing a shear force between filaments
- the thin filament slides 50-100 angstroms relative to the thick filament causing the actin and myosin proteins to detach.



The Huxley Model (1957)



[adapted from McMahon 1984]

let $0 \leq n(x) \leq 1$ be the probability that a crossbridge exists at displacement x , then

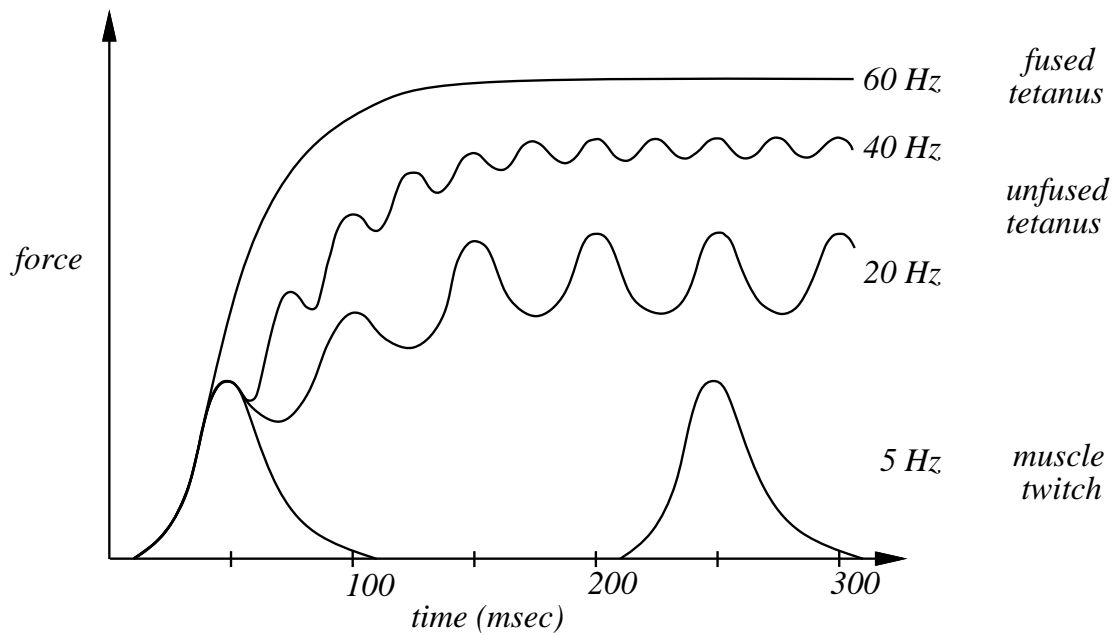
$$\frac{dn(x)}{dt} = [1 - n(x)] f(x) - n(x)g(x),$$

where $f(x)$ is the probability of a new attachment and $g(x)$ describes the probability that an existing crossbridge will detach.

The shape of functions $f(x)$ and $g(x)$ is chosen so that muscles tend to shorten in response to neural excitation.



Twitch and Tetanic Responses

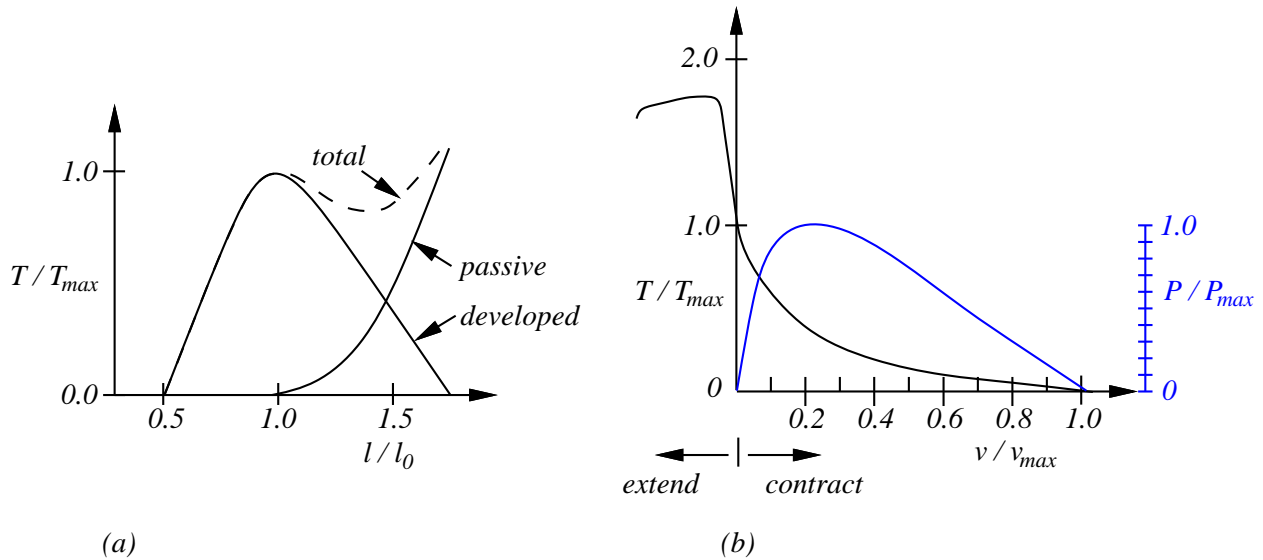


[adapted from McMahon 1984]

large mammalian muscles subject to periodic activation at 5, 20, 40, and 60 Hz.



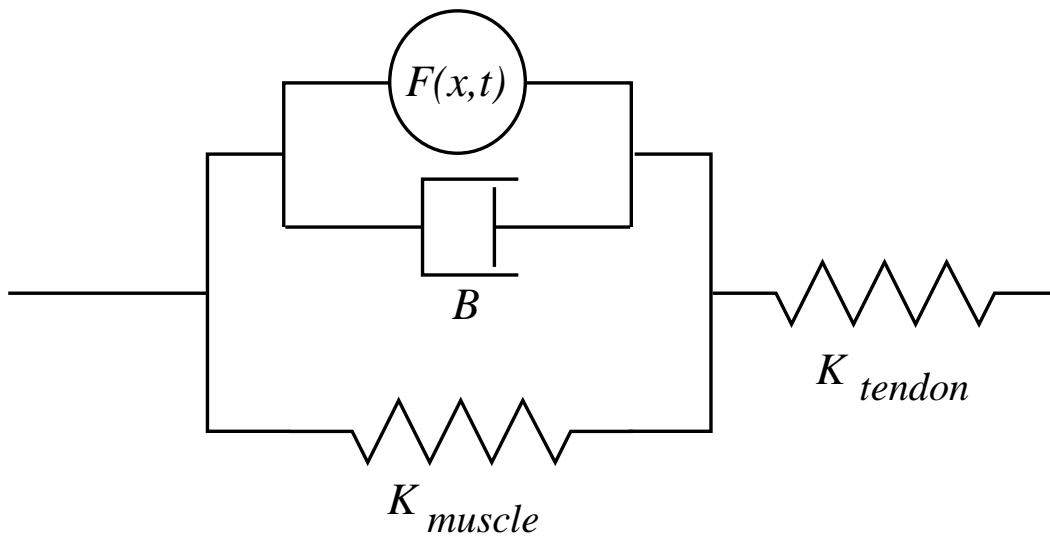
Muscle Force Generation



The force capacity of muscle as a function of length and velocity. Tension is normalized by the maximum developed tension, length by muscle free length (l_0), and velocity by the maximum unloaded contractile velocity (v_{max}).



Muscle: Linear Model

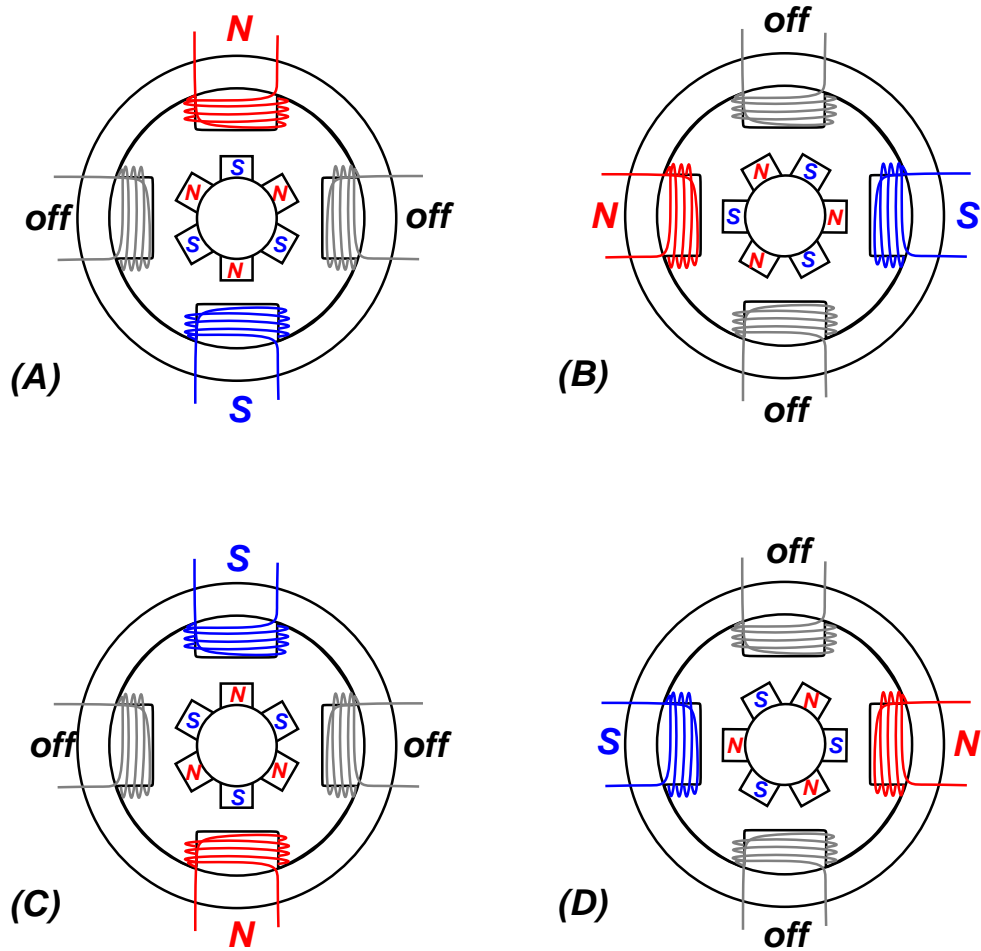


active and passive muscle dynamics



Actuators: Stepper Motors

- precise (low torque), open-loop position control
- *resonance* - typically between 50 and 150 *steps/sec*
- *cogging*

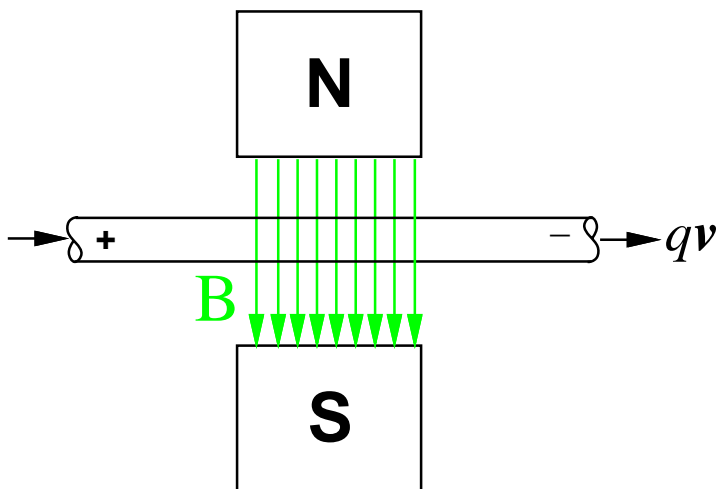




Permanent Magnet DC Motors

- run continuously in both directions
- closed-loop servo control w/position feedback
- reliable, good power/weight, high torques possible

Lorentz Force



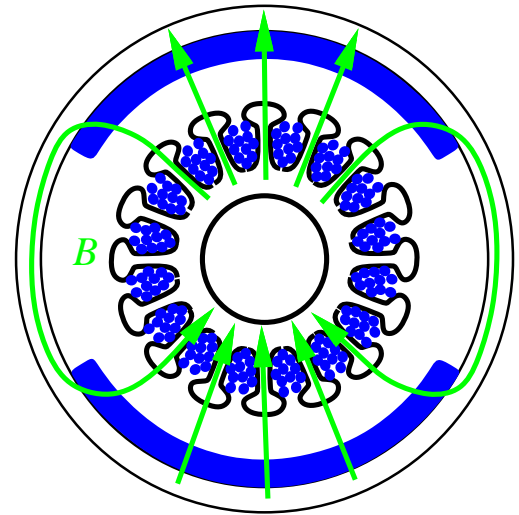
$$\mathbf{F} = q\mathbf{v} \times \mathbf{B}$$



Permanent Magnet DC Motor

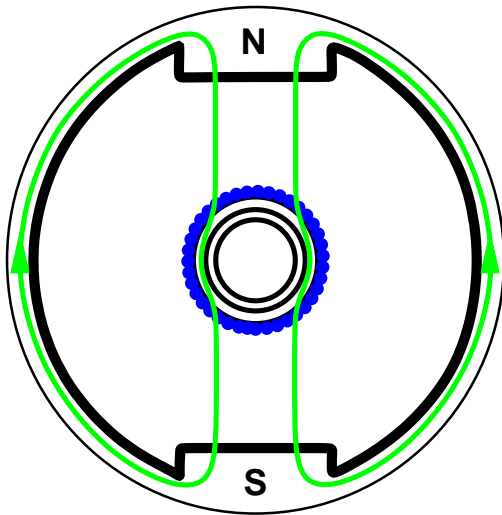
Iron Core:

- high inertia, cogging
- very reliable
- cheap



Moving Coil:

- rare earth magnets - coil *is* rotor
- low rotor inertia - minimal *cogging*
- large torque
- can be thin (0.02"), large diameter (12")
- *printed-circuit motors*
- very expensive





DC Motors - Electrodynamics

force: Newton $N = kg \cdot m/sec^2$

torque: the product of a force and a moment arm

$$N \cdot m = \frac{kg \cdot m^2}{sec^2}$$

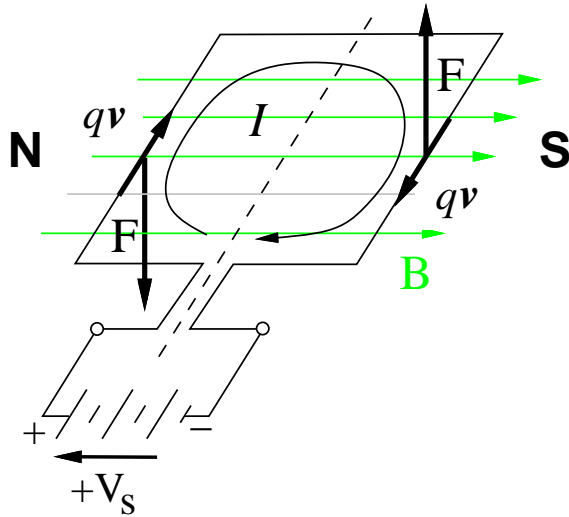
power: energy per unit time (Watts)

$$\begin{aligned} P &= VI(\text{electrical}) \\ &= \tau\omega(\text{mechanical}) \end{aligned}$$

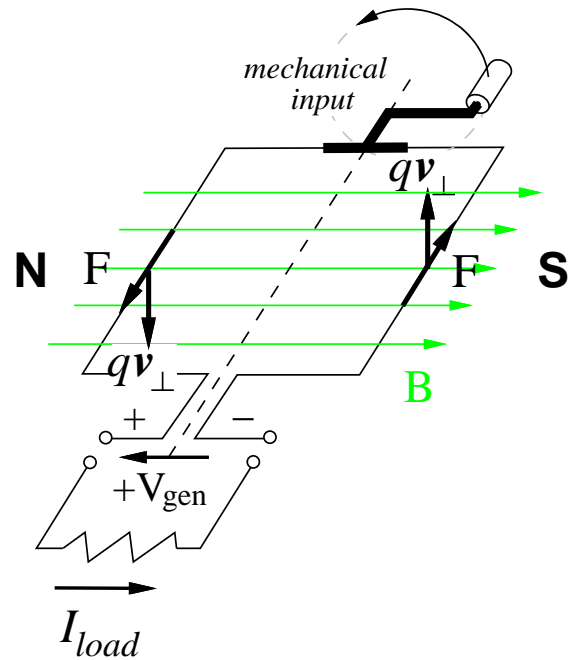
$$Watt = \frac{volt \cdot coulomb}{sec} = \frac{Nm}{sec}$$



DC Motors - Electrodynamics



The Lorentz Force

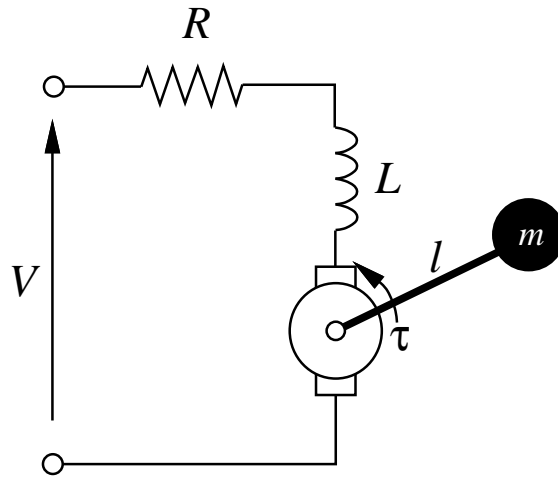


Backward Electromotive Force (Back EMF)

- commutation - the rotor runs out of torque when the current loop is perpendicular to B , reversing the current can continue to provide torque in the same direction.
- K_m : overall motor torque constant - total number of current loops, magnetic field strength, supply voltage, rotor resistance
 - torque production: $\tau = K_m I$
 - back emf: $V_b = K_m \omega$



DC Motors - Electrodynamics (cont.)



ignoring rotor inductance L

forward
current

$$\sum \tau = J\ddot{\theta} = K_m I = K_m \left[\frac{V}{R} - \frac{K_m \dot{\theta}}{R} \right]$$

back
current

$$\ddot{\theta} + \frac{K^2}{JR} \dot{\theta} + \frac{KV}{JR} = 0$$



DC Motor Performance

manufacturers publish physical parameters:

rotor inertia J , resistance R , inductance L , as well as overall mass and geometry of the motor package

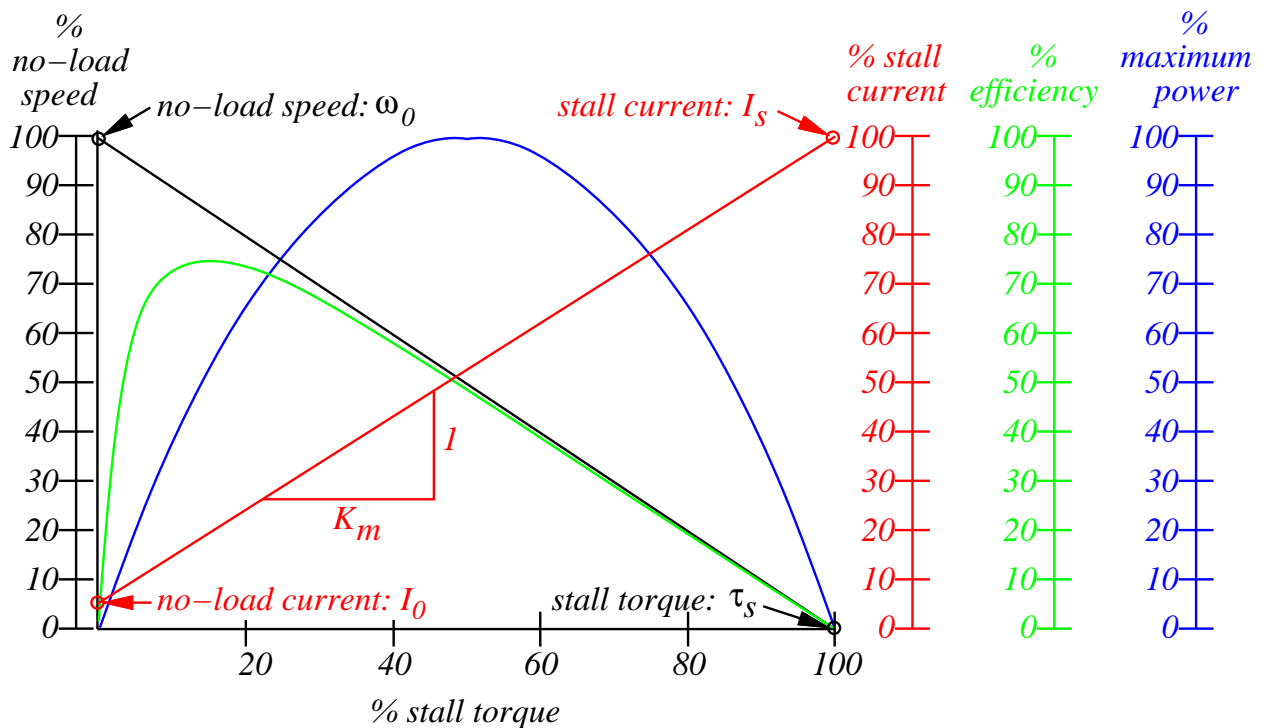
and integrated motor performance data:

ω_0 : no-load velocity

τ_s : stall torque

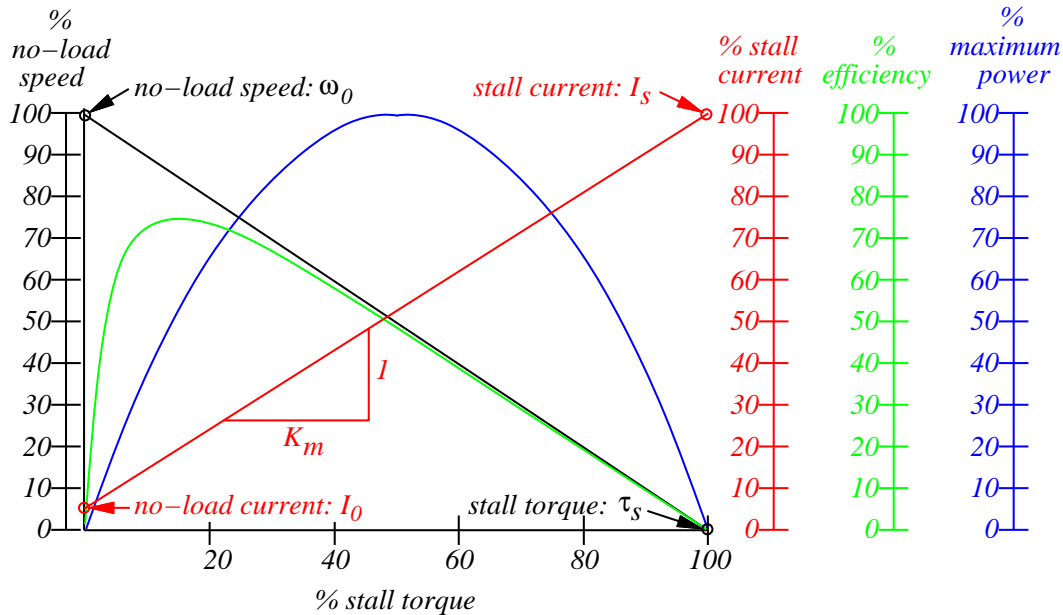
I_0 : no-load current

I_s : stall current





DC Motor Performance



Power: the product of torque and speed ($\tau\omega$) for loads $[0, \tau_s]$

$$P_{out} = \tau_{load} \omega_{\tau} = \tau_{load} \left[\omega_0 - \frac{\Delta\omega}{\Delta\tau} \tau_{load} \right] = - \left(\frac{\Delta\omega}{\Delta\tau} \right) \tau_{load}^2 + (\omega_0) \tau_{load}$$

Efficiency: $\eta_{\tau} = \frac{\text{mechanical power out}}{\text{electrical power in}} = \frac{P_{out}}{V_s I}$

$$\eta_{\tau} = \frac{- \left(\frac{\Delta\omega}{\Delta\tau} \right) \tau_{load}^2 + (\omega_0) \tau_{load}}{V (I_0 + \tau_{load}/K_m)}$$

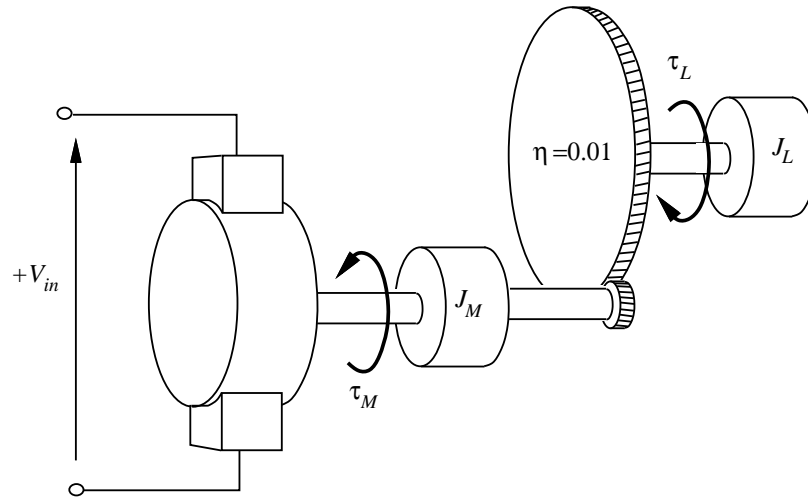


Roger's Motor Parameters

PARAMETER	wheel	shoulder	elbow	eye
ω_0 [rad/sec] no-load speed	175.0	30.1	50.3	122.2
I_0 [A] no-load current	0.38	0.26	0.17	0.12
τ_s [N · m] stall torque	475.0	205.3	120.7	2.7
K_m $\left[\frac{N \cdot m}{A}\right]$ $\left[\frac{V \cdot sec}{rad}\right]$ torque constant	0.105	0.623	0.364	0.163



DC Motors/Gearhead Combinations



if the transmission is perfectly efficient:

$$\tau_{out}\omega_{out} = \tau_{in}\omega_{in}$$

$$\tau_{out}(\eta\omega_{in}) = \tau_{in}\omega_{in}$$

$$\tau_{out} = (1/\eta)\tau_{in}$$

if $\eta = 0.01$, the output shaft carries one hundred times the torque at one hundredth the velocity of the input shaft



DC Motors/Gearhead Combinations — Compound Loads

dynamic equation of motion - equate the torque derived from Lorentz forces with the torques required to accelerate the load and to overcome viscous friction.

$$\tau_M = \left[J_M \ddot{\theta}_M \right] + \eta \left[J_L \ddot{\theta}_L \right]$$

but:

$$\begin{aligned} \theta_L &= \eta \theta_M, \\ \dot{\theta}_L &= \eta \dot{\theta}_M, \text{ and} \\ \ddot{\theta}_L &= \eta \ddot{\theta}_M \end{aligned}$$

so:

$$\tau_M = \left[J_M + \eta^2 J_L \right] \ddot{\theta}_M$$

and:

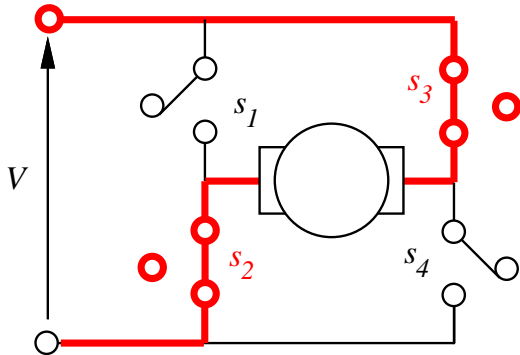
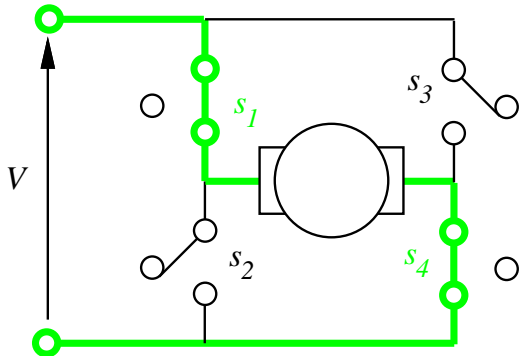
$$J_{eff} = J_M + \eta^2 J_L$$

if $\eta = 0.01$, this means the relative influence of the motor dynamics is amplified 10,000 fold



Driving DC Motors

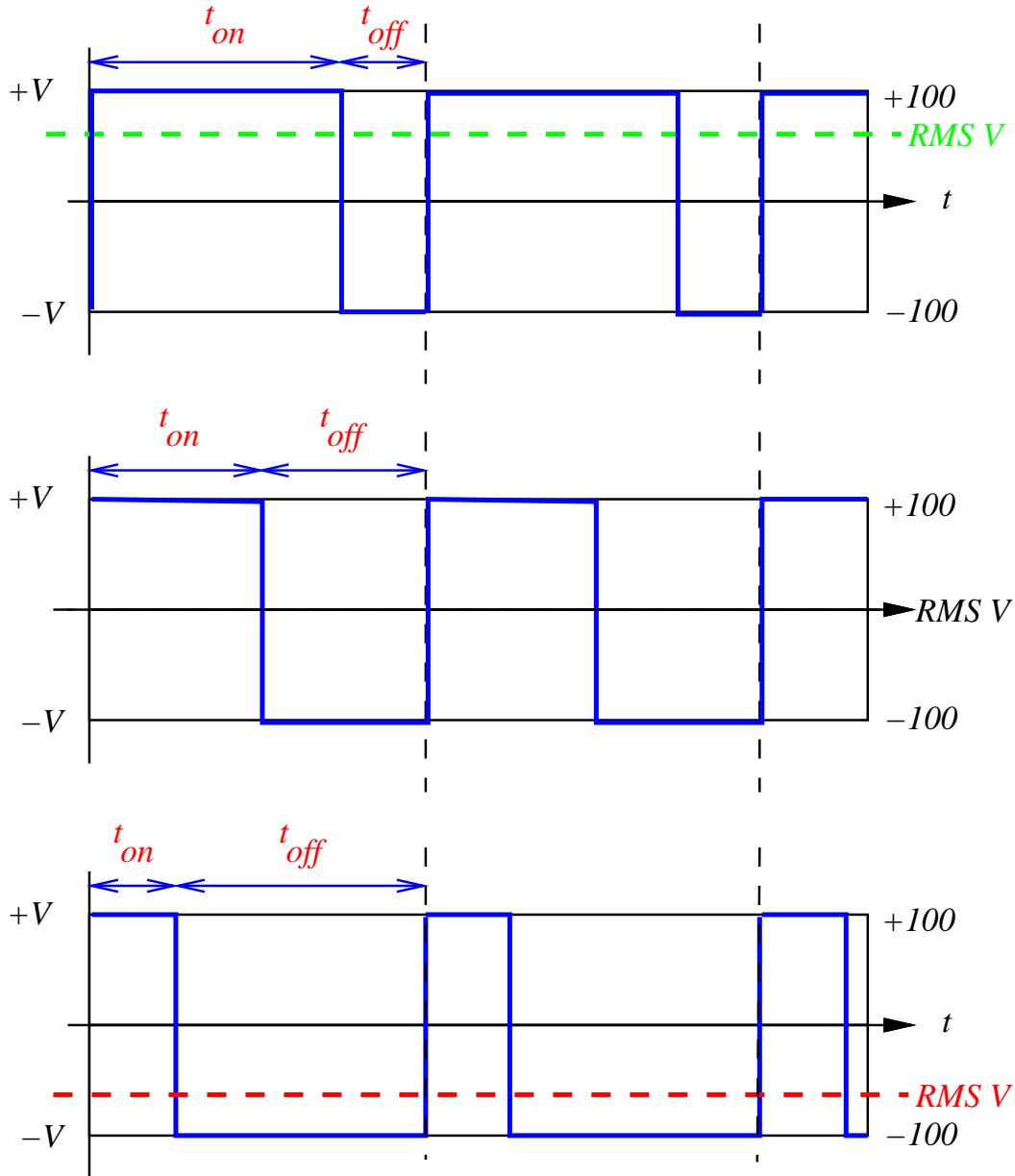
H-Bridge



- continuous forward/backward speed control
- (s_1, s_2, s_3, s_4) open - freewheel
- (s_1, s_2, s_3, s_4) closed - (regenerative) braking
- RMS voltages - pulse width modulation (PWM)

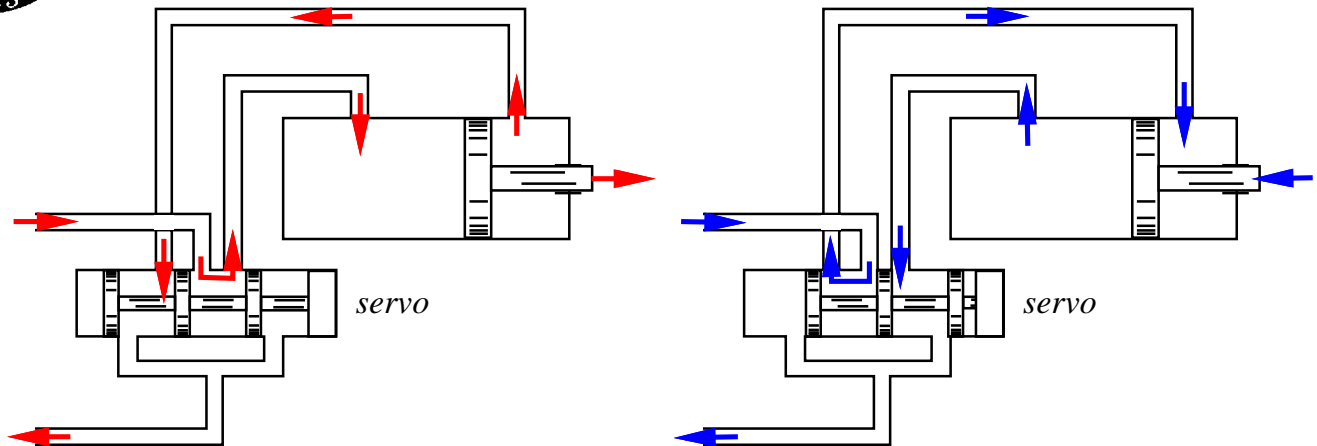


Pulse Width Modulation





Actuators: Hydraulic



- energy in the high pressure fluid reservoir (1000-3000 psi)
- open-loop control - fork lifts, back hoes
- good bandwidth (5 KHz - fluid reverses direction 5 msec)

PROS

1. good power/weight
2. safe in explosive environments

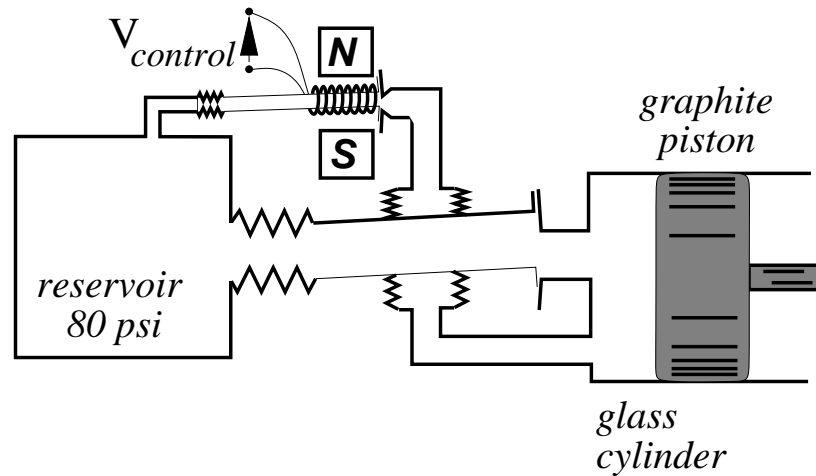
CONS

1. expensive servos
2. messy
3. high maintenance



Actuators: Pneumatic

- compressible fluid (air)
- jet-pipe servo control



PROS

1. light and cheap
2. passively backdrivable

CONS

1. stiction
2. delicate



Artificial Muscles

McKibben Air Muscles - non-linear pneumatic actuators, attract interest because they are among the strongest and fastest of the “artificial” muscles.

Shape Memory Alloys - Nitinol “muscle wire” (nickel-titanium alloy) relatively slow, commercially available, a few grams force (similar to all options below this on in the list), low bandwidth (1Hz)

Polymers - electrostatic, chemical, and thermal, polymer gels can exhibit abrupt, reversible 1000 fold volume changes, forces up to 100 N/cm^2 , contraction rates on the order of a second.

Synthetic Muscle - extracted actin and myosin protein, possibly avoiding tissue rejection

Bucky Tubes - Fullerenes (“Bucky Balls”) and nanotubes (“Bucky Tubes”), crystalline configurations of graphitic carbon.